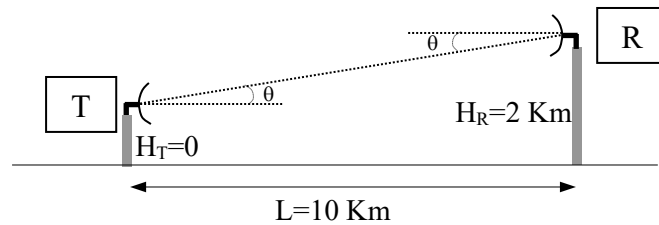


**RF SYSTEMS**  
**7<sup>th</sup> September 2020**

Exercise 1



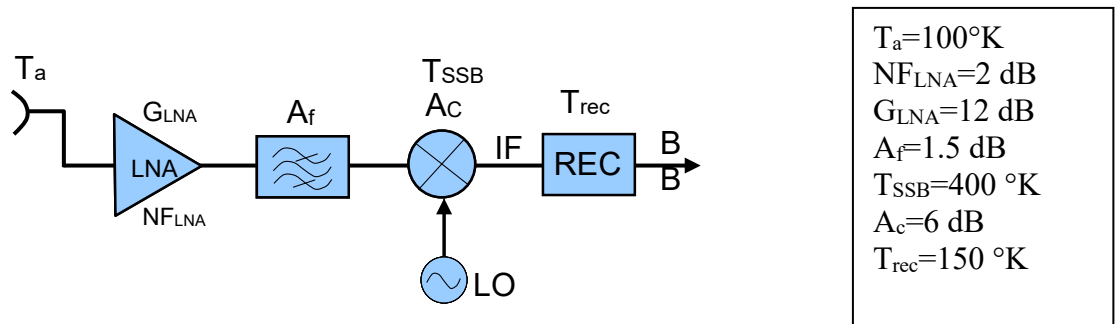
The transmitter operates at 10 GHz with a transmitted power  $P_T = 20 \text{ dBm}$ . The receiver is located 10 Km apart from the transmitter, placed at a height of 2000 m. The two antennas are equal, horizontally pointed and exhibit directivity function  $f(\phi, \theta) = \cos^4(\theta)$  for  $0 < \theta < \pi/2$ ,  $= 0$  elsewhere. The efficiency is  $\eta = 0.85$ .

- 1) Evaluate the gain  $G$  of the two antennas. Recall:  $\int f^n(x) f'(x) dx = \frac{f^{n+1}(x)}{n+1}$
- 2) Evaluate the power density  $S_R$  of the incident wave on the receiving antenna.
- 3) Assuming the radiation impedance of the antennas ( $Z_{\text{rad}}$ ) equal to 60 Ohm and the input impedance of the receiver ( $Z_L$ ) equal to 50 Ohm, evaluate the received power.

## Exercise 2

Consider the following scheme of a receiver operating at 4 GHz (signal band 50 MHz). The block REC represents the demodulator at intermediate frequency (IF), producing the bit streaming in base band (BB). It is characterized by the noise temperature  $T_{\text{rec}}$  (at input).

Assume that the filter eliminates completely the image band (no noise contribution at IF).

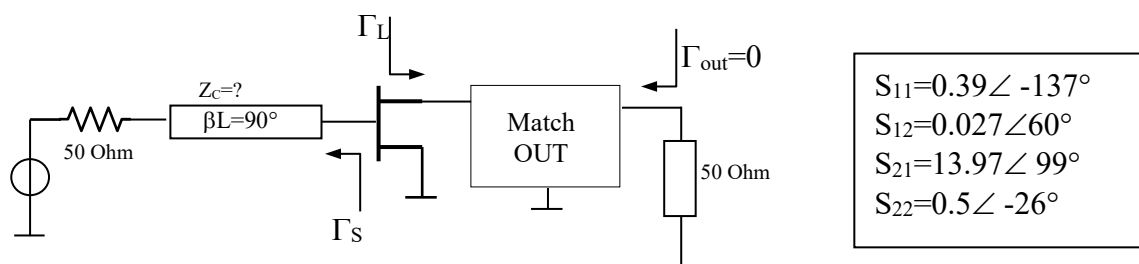


- 1) Evaluate the equivalent noise temperature at the input of the receiver ( $T_{\text{eq}}$ ).
- 2) Assuming  $E_b/N_0=20\text{ dB}$ , what is the minimum signal power at IF allowing a data rate  $R=100\text{ Mbit/sec}$ ?
- 3) What is the main drawback of connecting the antenna directly to the input of LNA? If the LNA is removed, what is the required input power to get the same data rate  $R$ ?

## Exercise 3

We want to design the amplifier in the figure operating at 500 MHz, with matching at output ( $\Gamma_{\text{out}}=0$ ). It is known that the Match OUT network is lossless.

The S parameters of the active device at 500 MHz are specified in the figure.



- 1) Evaluate  $\Gamma_S$  and  $\Gamma_L$  to get the highest transducer gain compatible with stability and matching requirement (the selected  $\Gamma_S$  must be realizable with the assigned input network). Specify the value of transducer gain. Hint: the requirement of matching at output suggests using the available gain for the amplifier design.
- 2) Evaluate the characteristic impedance  $Z_c$  of the input transmission line (must be larger than 25 Ohm).

## SOLUTION

### Exercise 1

1) The gain is expressed as follows:

$$G = \frac{4\pi\eta}{\int_{-\pi}^{\pi} \int_0^{\pi} f(\theta) \sin(\theta) d\varphi d\theta} = \frac{4\pi\eta}{2\pi \int_0^{\pi/2} \cos^4(\theta) \sin(\theta) d\theta} = \frac{2 \cdot 5 \cdot 0.85}{[-\cos(\theta)]_0^{\pi/2}} = 8.5 \quad (9.29 \text{ dB})$$

2) The power density at the receiving antenna position is given by  $SR = \frac{P_t}{4\pi R^2} G \cdot f(\theta)$ , with  $R^2 = 10^2 + 2^2 = 104 \text{ Km}^2$ ,  $\theta = \tan^{-1}\left(\frac{2}{10}\right) = 11.31^\circ$ . Replacing:  $SR = 6.0132 \cdot 10^{-10} \text{ W/m}^2$ .

3) The maximum received power  $P_{r,max}$  is given by  $P_{r,max} = SR \cdot A_e \cdot f(\theta)$ , with  $A_e = G \cdot \lambda^2 / 4\pi = 6.0877 \text{ m}^2$  and  $f(\theta) = \cos^4(11.31^\circ) = 0.9246$ . We get then  $P_{r,max} = 3.3845 \cdot 10^{-13} \text{ W}$ .

The power developed on the load is given by

$$P_L = P_{r,max} k_{mis}^2 = P_{r,max} \frac{4 \operatorname{Re}\{Z_{rad}\} \operatorname{Re}\{Z_L\}}{|Z_{rad} + Z_L|^2} = 3.3565 \cdot 10^{-13} \text{ W} \quad (-97.74 \text{ dBm})$$

### Exercise 2

1) The equivalent noise temperature at input is given by:

$$T_{eq} = T_a + T_{LNA} + \frac{1}{G_{LNA}} (T_f + A_f (T_{SSB} + T_{rec} A_c))$$

with:

$$T_{LNA} = 293(10^{NF/10} - 1) = 171.37 \text{ }^\circ\text{K}, \quad A_f = 10^{1.5/10} = 1.4125, \quad T_f = 293(10^{A_f/10} - 1) = 120.87 \text{ }^\circ\text{K}$$

$$G_{LNA} = 10^{12/10} = 15.85, \quad A_c = 10^{6/10} = 4$$

Replacing:  $T_{eq} = 368.11 \text{ }^\circ\text{K}$ .

2) The received power is determined by the required SNR:

$$SNR = \frac{P_r}{KT_{eq}B} = \frac{E_b}{N_0} \frac{R}{B} \Rightarrow P_r = (KT_{eq}B) \frac{E_b}{N_0} \frac{R}{B} = 2.54 \cdot 10^{-13} \cdot 100 \cdot 2 = 5.08 \cdot 10^{-11} \text{ W} \quad (-72.94 \text{ dBm})$$

The power at IF is then given by:

$$P_{IF} = P_r \frac{G_{LNA}}{A_c A_f} = 2.8 \cdot P_r = 1.425 \cdot 10^{-10} \quad (-68.46 \text{ dBm})$$

3) Removing the LNA the  $T_{eq}$  becomes:

$$T_{eq} = T_a + T_f + A_f (T_{SSB} + T_{rec} A_c) = 1633.4 \text{ }^\circ\text{K}$$

Then the received power must be increased to  $P'_r = P_r \cdot 1633.4 / 368.11 = 2.254 \cdot 10^{-10} \text{ W} \quad (-66.47 \text{ dBm})$

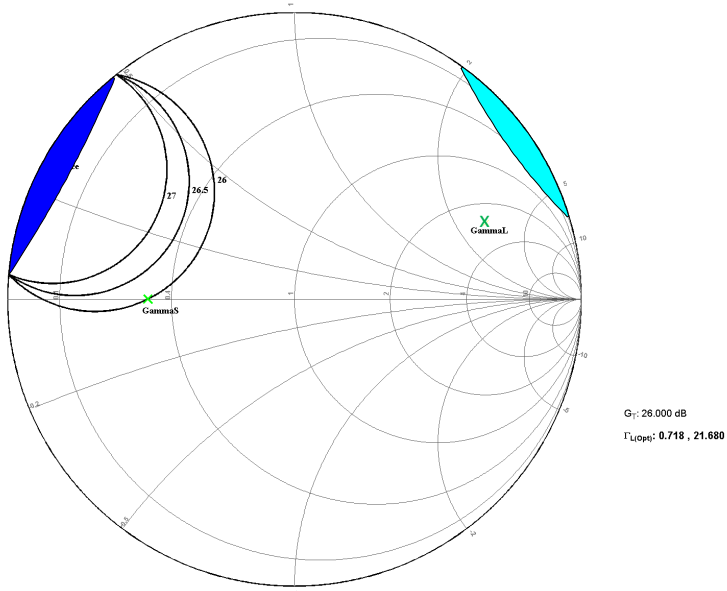
### Exercise 3

Active device: potentially unstable (MSG=27.14 dB)

To get the output matched we chose  $\Gamma_s$  for the maximum available gain, compatible with the required condition ( $\Gamma_s$  must be real to be realized with the assigned input network). We then draw on the S. C. some circles with  $G_{av} = \text{const}$  (starting with  $G_{av} = 27 \text{ dB}$ ), until the circle crosses the horizontal axis. The point to be selected for  $\Gamma_s$  is just the intersection with this axis (see the following figure). Finally

we get:  $\Gamma_s = -0.511$  with  $G_{av} = 26$  dB. Imposing conjugate matching at the transistor output we get  $\Gamma_L = 0.718 \angle 21.68^\circ$ .

Note that both  $\Gamma_s$  and  $\Gamma_L$  are outside the forbidden regions (potential instability).



2) From  $\Gamma_s = -0.511$  we get  $R_s = 0.323 \cdot 50 = 16.15$  Ohm. Then the characteristic impedance of the  $\lambda/4$  transformer is given by  $Z_c = \sqrt{Z_0 \cdot R_s} = 28.42$  Ohm ( $> 25$  as required) .