

**RF SYSTEMS**  
**Written Test of February 11, 2021**

Exercise 1

A satellite earth station operates at 6 GHz (uplink) with a geostationary satellite (assume the link length equal to 36000 Km). The earth antenna has the following directivity function:  $f_T = \cos(110^\circ \theta_T)$  ( $\theta < \pi/200$ ),  $f_T = 0$  ( $\theta > \pi/200$ ). The transmitted power from earth is 5 KW.

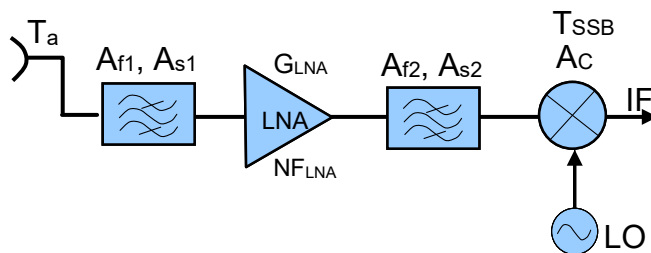
- a) Evaluate the directivity gain of the earth antenna. Hint:

$$\int \sin(x) \cos(nx) dx = \frac{\cos((n-1)x)}{2n-2} - \frac{\cos((n+1)x)}{2n+2}$$

- b) Evaluate the gain of the antenna satellite so that the received power is at least -65 dBm. Verify that the beamwidth of the antenna corresponding to the computed gain is sufficient to cover the portion of Earth seen by the satellite (assume for the satellite antenna  $f(\theta) = 1$  inside the beam and the efficiency of both antennas equal to 1)

Exercise 2

Consider the following scheme of a receiver front-end operating in the band 10-10.5 GHz (signal bandwidth 10 MHz). Note that the filters are characterized by a finite attenuation  $A_S$  in the stopband (which coincides with the image band of the receiver), in addition to the attenuation  $A_f$  in the passband.



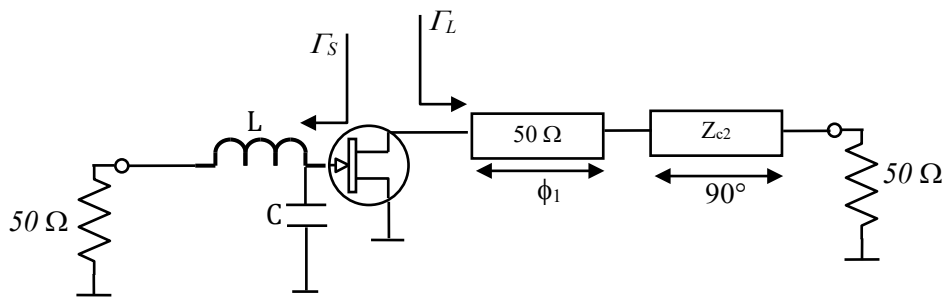
$T_a = 100^\circ\text{K}$
$A_{f1} = 1 \text{ dB}, A_{s1} = 10 \text{ dB}$
$NF_{LNA} = 2 \text{ dB}$
$G_{LNA} = 10 \text{ dB}$
$A_{f2} = 2 \text{ dB}, A_{s2} = 15 \text{ dB}$
$T_{SSB} = 350^\circ\text{K}$
$A_c = 6 \text{ dB}$

- 1) Assuming the local oscillator tunable in the range 11-11.5 GHz, specify the limits of the image band and the value of the intermediate frequency.
- 2) Draw the equivalent scheme for the evaluation of the noise temperature and evaluate of the equivalent noise temperature at the input of the receiver (assume  $T_0 = 293^\circ\text{K}$ ).
- 3) Assuming  $E_b/N_0 = 20 \text{ dB}$ , what is the minimum signal power at IF (in dBm) allowing a data rate  $R = 20 \text{ Mbit/sec}$ ?

### Exercise 3

The following scheme represents an amplifier operating at 20 GHz. The active device (whose S parameters are given below) is unconditionally stable with  $G_{Tmax}=12.9$  dB. The following constraint is imposed on the reflection coefficient at the input of the device:  $|\Gamma_s| \leq 0.5$ .

- Determine the values  $\Gamma_s$  and  $\Gamma_L$  so that the transducer gain of the amplifier is maximum (compatibly with the imposed constraint)
- Compute the parameters of the input and output matching networks.

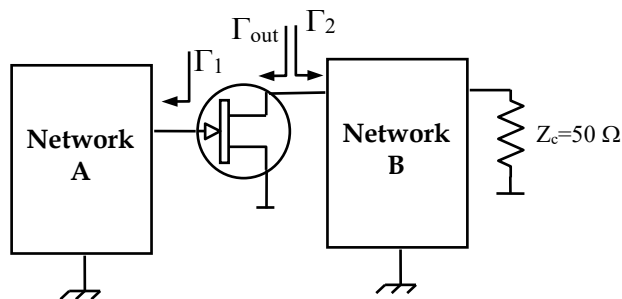


Scattering and noise parameters of the transistor:

$$S_{11}=0.642 \angle 47.3^\circ \quad S_{21}=2.934 \angle -79.2^\circ \quad S_{12}=0.107 \angle -75.2^\circ \quad S_{22}=0.204 \angle 67.8^\circ$$

### Exercise 4

The following figure represents the general configuration of a microwave oscillator. Using the reported scattering parameters of the active device, evaluate the reflection coefficients  $\Gamma_1$  and  $\Gamma_2$  which ensure the start of oscillation (the magnitude of  $\Gamma_1$  must be imposed equal to 1. Assume  $|\Gamma_{out}|=1.2$ ).



$$\begin{aligned} S_{11} &= 0.69 \angle -55^\circ \\ S_{12} &= 0.026 \angle 64.7^\circ \\ S_{21} &= 27.5 \angle 146.3^\circ \\ S_{22} &= 0.82 \angle -35.7^\circ \end{aligned}$$

## Solution

### Exercise 1

1) Directivity gain:

$$D_M = 4\pi \left[ \int_0^{2\pi} d\varphi \int_0^{\pi} f(\theta) \sin \theta d\theta \right]^{-1} = \frac{2}{\int_0^{\pi/200} \sin(\theta) \cos(110 \cdot \theta) d\theta} = \frac{2}{\left[ \frac{\cos(109 \cdot \theta)}{218} - \frac{\cos(111 \cdot \theta)}{222} \right]_0^{\pi/200}} =$$

$$= \frac{2}{4.5468 \cdot 10^{-5}} = 4.4 \cdot 10^4 \text{ (46.4 dB)}$$

2) Friis equation of the link ( $\lambda=c/f=0.05\text{m}$ ):

$$P_r = P_t + G_E + G_S - 20 \log \left( \frac{4\pi R}{\lambda} \right)$$

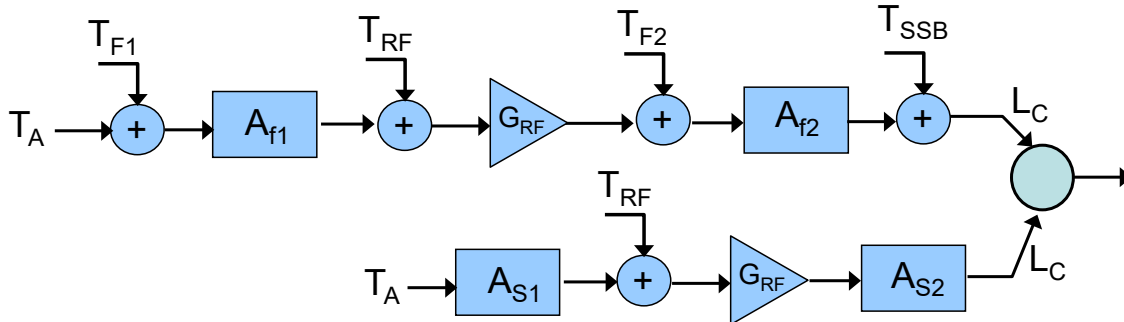
Assigning  $P_r=-65 \text{ dBm}$ , we get  $G_S=-65-67-46.4+199.13=20.73 \text{ dB}$

Assuming unitary the directivity function:

$$\theta_B = \cos^{-1} \left( 1 - \frac{2}{D_S} \right) = 10.55^\circ \Rightarrow \Delta\theta = 2\theta_B = 21.1^\circ \quad (>17.36^\circ)$$

### Exercise 2

- 1) The intermediate frequency (IF) is given by  $f_{RF}-f_{OL}=1 \text{ GHz}$ . The image band is then given by  $f_{\text{image}}=f_{OL}+f_{IF}=12-12.5 \text{ GHz}$ .
- 2) Equivalent scheme for the evaluation of the Noise Temperature:



Note that the two filters do not produce noise in the image band because the attenuation is generated by reflection in the filter stopband.

Evaluation of  $T_{eq}$ :

$$T_{F1} = 293 \left( 10^{\frac{A_{f1}}{10}} - 1 \right) = 75.86^\circ K, \quad T_{F2} = 293 \left( 10^{\frac{A_{f2}}{10}} - 1 \right) = 171.37^\circ K, \quad T_{RF} = 293 \left( 10^{\frac{NF}{10}} - 1 \right) = 171.37^\circ K$$

$$T_{eq} = T_a + T_{F1} + T_{RF} A_{f1} + T_{F2} \frac{A_{f1}}{G_{RF}} + T_{SSB} \frac{A_{F1} A_{F2}}{G_{RF}} + T_A \frac{A_{f1} A_{f2}}{A_{S1} A_{S2}} + T_{RF} \frac{A_{f1} A_{f2}}{A_{S2}} = 494.45^\circ K$$

3) Evaluation of  $P_{IF}$ :

$$SNR_{sys} = \frac{P_r}{KT_{eq}B} = \left( \frac{E_b}{N_0} \right) \frac{R}{B} = 20 + 10 \log(20/10) = 23 \text{ dB}$$

$$KT_{eq}B = 1.38 \cdot 10^{-23} \cdot 494.45 \cdot 10 \cdot 10^6 = 6.82 \cdot 10^{-14} \text{ (-101.66 dBm)}$$

$$P_r = SNR_{sys} + KT_{eq}B \Big|_{dBW} = -108.65 \text{ dBW}$$

$$P_{IF} = P_r - A_{f1} + G_{LNA} - A_{f2} - A_c = -77.65 \text{ dBm}$$

### Exercise 3

- 1) To get  $\Gamma_S$  we draw first the circle  $|\Gamma_S|=0.5$ . Then we draw some circle with  $G_{AV}=\text{const.}$  until we find the one tangent to the previous circle. We get  $\Gamma_S=0.5\angle 53^\circ$  and  $G_{AV}=11.93 \text{ dB}$ . To get the maximum gain we find  $\Gamma_L$  so that the output is matched:  $\Gamma_L=0.328\angle -111.9^\circ$ . With this choice  $G_T=G_{AV}=11.93 \text{ dB}$ .
- 2) For the input matching network we start from  $\Gamma_S$  as current point and draw the circle  $g=\text{const}$  passing for it. Then we draw the circle  $r=1$  and select the intersection for which  $\Delta B$  is negative (C is removed from what we observe in the direction of load):  $b_C=-\Delta B=0.922$ . In the intersection point what we observe is the impedance in the load direction, that is  $z=1+jx_L$ . The current point gives then  $x_L=1.213$ . The values of C and L are obtained by de-normalizing  $b_C$  and  $x_L$ :  $C=0.02 \cdot b_C / 2\pi f = 0.147 \text{ pF}$ ,  $L=50 \cdot x_L / 2\pi f = 0.48 \text{ nH}$ .  
The output network requires that the impedance seen at the input of the second transmission line is real. Then we start from  $\Gamma_L$  (current point) and draw the circle  $|\Gamma|=\text{const}$ . The first intersection with the horizontal axis in the load direction defines the length of the first line:  
 $\phi_1=111.9/2=55.95^\circ$ . The impedance in this point is also the input impedance of the second line:  
 $z_{in}=1.98$ . De-normalizing:  $Z_{in}=50 \cdot z_{in}=99 \text{ Ohm}$ . For the property of the  $\lambda/4$  inverter:  
 $Z_{c2}=\sqrt{50 \cdot 99}=70.36 \text{ Ohm}$ .

### Exercise 4

We draw the mapping circle of source with  $|\Gamma_{out}|=1.2$  and select one of the two points intersecting the unit circle:  $\Gamma_1=1\angle 143.3^\circ$ . Then we get  $z_{out}=-6.4-j5.39$ . We assign  $z_L=r_{out}/3-x_{out}=2.1+j5.39$  corresponding to  $\Gamma_2=.885\angle 18.37^\circ$ .