

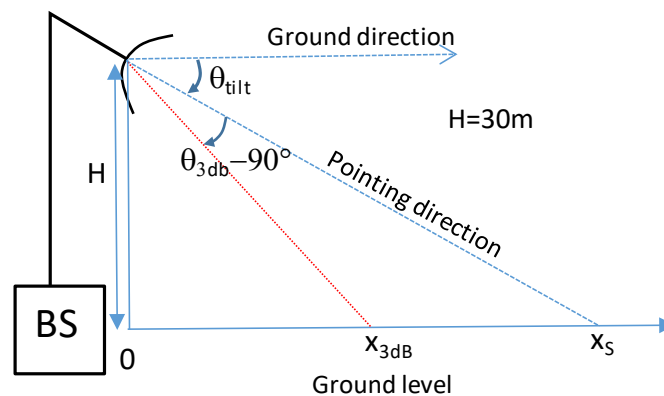
RF SYSTEMS

Written Test of June 20, 2019

Surname & Name
Identification Number
Signature

Exercise 1 (8+2)

Consider the antenna used in a base station for LTE service, placed at $H=30$ m above ground. The operating (downlink) frequency is $f_0=2.12$ GHz.



The directivity function is expressed as:

$$f(\varphi, \theta) = f_\varphi(\varphi) \cdot f_\theta(\theta) \quad \varphi: \text{azimuth}, \theta: \text{elevation}$$

$$f_\varphi(\varphi) = \cos(\varphi) \quad -\pi/2 \leq \varphi \leq \pi/2, \quad 0 \text{ elsewhere}$$

$$f_\theta(\theta) = \sin(5\theta) \quad 2\pi/5 \leq \theta \leq 3\pi/5, \quad 0 \text{ elsewhere}$$

Note that angles θ and φ refer to the pointing direction ($\theta=90^\circ$, $\varphi=0^\circ$). This direction is tilted by θ_{tilt} with respect to the direction parallel to ground in order to reduce the interference among adjacent cells.

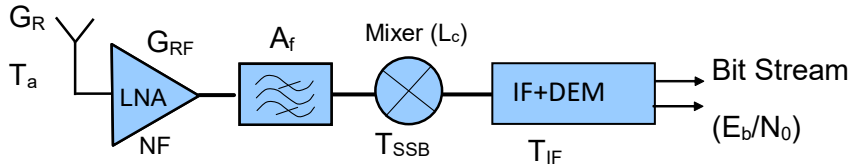
- 1) Specify the angles θ_{max} and φ_{max} where $f(\theta, \varphi)$ is maximum
 - 2) Compute the antenna gain (efficiency factor $\eta=0.85$).
- Hint: $\int \sin(x) \sin(5x) = \frac{\sin(4x)}{8} - \frac{\sin(6x)}{12}$
- 3) x_S represents the distance from the base station at ground level determined by antenna tilting (see the figure). Imposing $x_S=1.5$ Km, determine the value of θ_{tilt}
 - 4) The transmitter power level is 30 dBm. Evaluate the power density (W/m^2) at x_S (with $\varphi=\varphi_{\text{max}}$).

(Optional)

- 5) Evaluate the angles $\theta_{3\text{dB}}$ and $\varphi_{3\text{dB}}$ where f_φ and f_θ are reduced by -3dB with respect to the optimum pointing (Hint: there are two values for each angle)
- 6) Evaluate also the power density at $x_{3\text{dB}}$ (the point at ground level determined by $\theta_{3\text{dB}}$). Assume $\varphi=\varphi_{3\text{dB}}$

Exercise 2 (8)

The scheme in the figure represents the RF front-end of a phone receiver using the BS of the previous exercise.



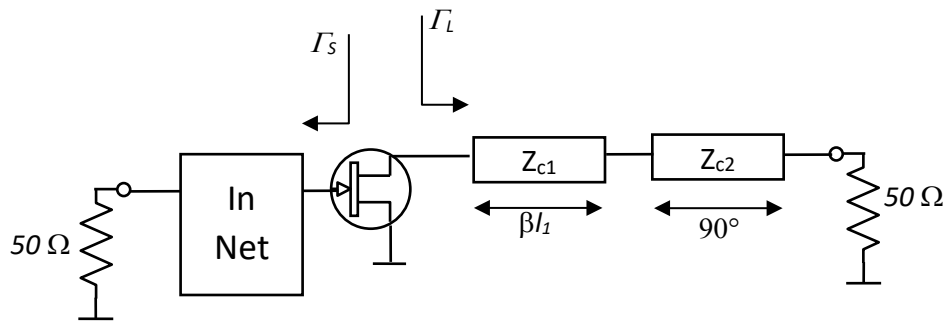
$G_R=1\text{dB}$
$NF=7$
$G_{RF}=10\text{ dB}$
$T_a=300\text{ }^\circ\text{K}$
$A_f=2\text{ dB}$
$L_c=6\text{ dB}$
$T_{SSB}=500\text{ }^\circ\text{K}$
$T_{IF}=500\text{ }^\circ\text{K}$

- Draw the scheme of the receiver referred to the equivalent noise sources. Evaluate the equivalent noise temperature (T_{eq}) at the receiver input. Compute the noise power at the receiver input (assume $B=20\text{ MHz}$). Use $K=1.38 \cdot 10^{-23}$ (Boltzmann Constant)
- Write the expression of the received power (at the antenna output) as function of the distance R from the BS
- It is requested the data rate $R=300\text{ Mbit/sec}$, with $(E_b/N_0)=10\text{ dB}$. Evaluate the corresponding SNR of the receiver.
- Evaluate the maximum distance R from the BS at which the data rate R is still guaranteed.

Exercise 3 (8)

The following scheme represents an amplifier operating at 12 GHz.

- Determine the values Γ_s and Γ_L for the maximum transducer gain
- Evaluate the unknown parameters (Z_{c1} , Z_{c2} , β_{l1}) of the output matching network

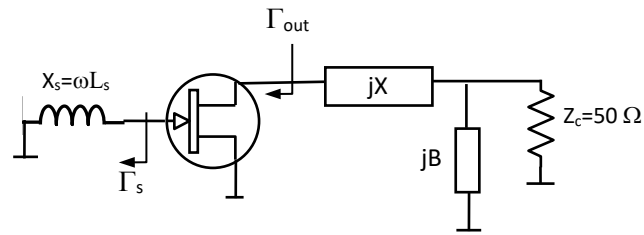


Scattering parameters of the transistor:

$$S_{11}=0.66\angle 146^\circ \quad S_{21}=2.39\angle 45^\circ \quad S_{12}=0.088\angle 69^\circ \quad S_{22}=0.3\angle -48^\circ$$

Exercise 4 (9)

The following scheme refers to an oscillator working at 432 MHz. The S parameters of the transistor are also reported on the figure.



$$S_{11} = 0.54 \angle -90^\circ$$

$$S_{12} = 0.01 \angle 66^\circ$$

$$S_{21} = 45.38 \angle 137^\circ$$

$$S_{22} = 0.76 \angle -26^\circ$$

- 1) Select a suitable value for L_s (use the mapping circles of Γ_s for obtaining $|\Gamma_{out}| = 1.5$)
- 2) Evaluate the parameters of the output network (jX , jB) to ensure the start of oscillation and the transfer of the output power to the external load (50Ω).
- 3) Find the values of the lumped elements parameters implementing X and B (select an inductor or a capacitor depending on the sign of X and B)

Solution

Exercise 1

1) $\theta_{\max}=90^\circ$, $\varphi_{\max}=0^\circ$

2) The antenna gain is obtained from the formula:

$$G = \eta 4\pi \left[\int_0^{2\pi} d\varphi \int_0^\pi f(\theta) \sin\theta d\theta \right]^{-1} = \frac{4\pi\eta}{\int_{-\pi/2}^{\pi/2} \cos(\varphi) d\varphi \int_{2\pi/5}^{3\pi/5} \sin(5\theta) \sin(\theta) d\theta} = \frac{4\pi\eta}{0.7925} = 13.4773$$

3) $x_s = H \cdot \tan(90 - \theta_{\text{tilt}}) \Rightarrow \theta_{\text{tilt}} = 90 - \tan^{-1}\left(\frac{x_s}{H}\right) = 1.146^\circ$

$$R_s = \frac{x_s}{\cos(\theta_{\text{tilt}})} = 1500.3 \text{ m}$$

4) $S_R = \frac{P_T G}{4\pi R_s^2} = \frac{1 \cdot 13.4773}{4\pi \cdot 1500.3^2} = 4.765 \cdot 10^{-7} \text{ W/m}^2$

$$f_\varphi(\varphi_{3dB}) = 0.5 \Rightarrow \varphi_{3dB} = \pm \pi/3$$

5) $f_\theta(\theta_{3dB}) = 0.5 \Rightarrow \theta_{3dB} = \frac{1}{5} \left(\frac{\pi}{6} + 2\pi \right) = \frac{13}{30} \pi$
 $= \frac{1}{5} \left(\frac{5\pi}{6} + 2\pi \right) = \frac{17}{30} \pi$

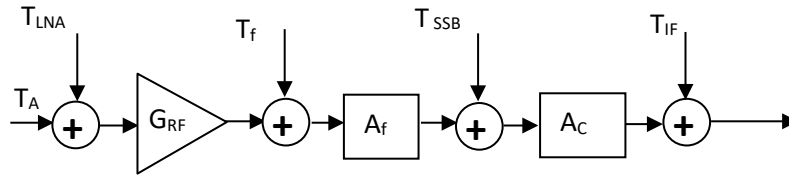
The above angles are those referred to the antenna pointing. Taking into account the tilting, the angle θ'_{3dB} with respect the absolute coordinate is given by $\theta'_{3dB} = \theta_{3dB} + \theta_{\text{tilt}}$

6) The distance R_{3dB} is given by: $R_{3dB} = H / \cos(\theta'_{3dB} - 90) = 131.9 \text{ m}$. Then:

$$S_{R_{3dB}} = \frac{P_T G}{4\pi R_{3dB}^2} f(\theta_{3dB}) f(\varphi_{3dB}) = 1.548 \cdot 10^{-5} \text{ W/m}^2$$

Exercise 2

a) Equivalent noise scheme :



Where:

$$T_f = 293 \left(10^{\frac{A_f}{10}} - 1 \right) = 171.4 \text{ °K}, \quad T_{LNA} = 293 \left(10^{\frac{NF}{10}} - 1 \right) = 1175.5 \text{ °K}$$

The equivalent noise temperature at the input of the receiver is then given by:

$$T_{eq} = T_A + T_{LNA} + \frac{T_f}{G_{RF}} + \frac{T_{SSB} A_f}{G_{RF}} + \frac{T_{IF} A_c A_f}{G_{RF}} = 1887.3 \text{ °K}$$

$$P_N = KT_{eq}B = 5.21 \cdot 10^{-13} \text{ W}$$

b) Friis equation:

$$P_r = P_T \cdot \left(\frac{\lambda}{4\pi R} \right)^2 \cdot G_T \cdot G_R = 0.002152/R^2$$

c) Evaluation of SNR:

$$SNR = \frac{P_r}{P_N} = \left(\frac{E_b}{N_0} \right) \left(\frac{R}{B} \right) = 150$$

d) Evaluation of the distance R:

$$P_r = SNR \cdot P_N = 7.815 \cdot 10^{-11} = 0.002152/R^2$$

$$R = \sqrt{\frac{0.002152}{7.815 \cdot 10^{-11}}} = 5.248 \text{ Km}$$

Exercise 3

The transistor is unconditionally stable with $G_{max}=12.1$ dB.
The optimum gamma are: $\Gamma_S=0.84 \angle -147.5^\circ$, $\Gamma_L=0.69 \angle 40.8^\circ$.
 $\beta I_L = 139.2/2=69.6^\circ$, $Z_{c1}=50\Omega$.

$$Z_{in} = 50 \cdot 0.18 = 9.05$$

$$Z_{c2} = \sqrt{Z_{in} \cdot 50} = 21.27 \Omega$$

Exercise 4

The mapping circle of Γ_S is drawn on the S.C with $|\Gamma_{out}|=1.5$. The two intersections with the outer circle are: $\Gamma_1=1 \angle 120.36$, $\Gamma_2=1 \angle 81.54$.

We assign $\Gamma_S = \Gamma_2$, from which $Z_s = j1.16 \cdot 50 = j58 \Omega$. The inductance L_s is then derived as:

$$L_s = \frac{X_s}{2\pi f_0} = 21.37 \text{ nH}$$

At the transistor out we get $\frac{Z_{out}}{50} = -0.726 - j1.5$.

Imposing: $Z_L = \frac{-\text{Re}(Z_{out})}{3} - \text{Im}(Z_{out})$ we get $Z_L = 50(0.24 + j1.5)$.

The design of the matching network can be carried out either with the S.C. or by means of the formulas. The following results are obtained:

$$X = 1.073 \cdot 50 = 53.64 \Omega, B = -1.776/50 = -0.03552 \text{ S}.$$

The lumped components value is then computed as follows:

$$L_X = \frac{|X|}{2\pi f_0} = 19.76 \text{ nH}$$

$$L_B = \frac{1}{|B|2\pi f_0} = 10.37 \text{ nH}$$