# **RF SYSTEMS** Written Test of June 23, 2021

Surname & Name	
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Exercise 1

A vehicle moving in the *x* direction is initially connected to the mobile network through the base station BS<sub>1</sub>. At the position  $x_A$  the connection switch to the base station BS<sub>2</sub> (*handover*). The two base stations have equal antennas with gain G<sub>BS</sub>=5.5 dB and the following directivity function ( $\varphi$  is the azimuthal angle and  $\theta$  is the elevation angle):

 $f(\theta, \varphi) = \cos^2(\varphi) \quad \text{for } 0 < \theta < \pi/2, \ -\pi/2 < \varphi < \pi/2$  $f(\theta, \varphi) = 0 \quad \text{elsewhere}$ 

Note that the directivity is constant along  $\theta$  (the plane in which the vehicle is moving is  $\theta=0$ ).

The transmitted power from BS<sub>1</sub> is  $P_{T1}=50W$  and the one from BS<sub>2</sub> is  $P_{T2}=20W$ . The downlink frequencies are 1.81 GHz (BS<sub>1</sub>) and 1.87 GHz (BS<sub>2</sub>).

It is known that the handover happens when the signals received by the vehicle from the two base stations have the same power ( $P_{RH}$ ).

- 1) (Mandatory, 7p) Evaluate the position  $x_A$  and the power  $P_{RH}$  at the handover. Assume the antenna on the vehicle omni-directional ( $f(\phi)=1$ ), with gain G<sub>A</sub>=2dB. Hint: the solution is found by equating at  $x_A$  the power  $P_{r1}$  received from BS<sub>1</sub> to the power  $P_{r2}$  from BS<sub>2</sub>.  $P_{r1}$  and  $P_{r2}$  are computed by means of the Friis equation.
- 2) (4p) Evaluate the directivity gain D and the efficiency  $\eta$  of the antennas used by the base stations. Hint:  $\int \cos^2(x) dx = x/2 + \sin(2x)/4$



### Exercise 2



Consider the scheme in the figure, which refers to RF front-end of a digital communication system operating at 6.4 GHz with a signal bandwidth B=32 MHz. All the relevant parameters of the system are reported in the scheme (except G<sub>LNA</sub> to be assessed).

- 1) (Mandatory, 6.5p) Assuming the received power  $P_r$ =-70 dBm and the required SNR=28 dB, evaluate the equivalent noise temperature  $T_{eq}$  of the RF front-end and the value of  $G_{LNA}$
- 2) (1p) Evaluate the required  $E_b/N_0$  to achieve 100 Mbit/sec at baseband
- 3) (3.5p) If the LNA and the second filter are removed, what is the new value of T<sub>SSB</sub> for maintaining T<sub>eq</sub> unchanged?

# Exercise 3

We want design a single stage amplifier at 12 GHz using the scheme in the following figure (input and output networks are lossless):



The amplifier must exhibit the transducer gain as high as possible compatibly with the stability requirement and the noise figure not larger than 1.5 dB.

- 1) (Mandatory, 6p) Select a proper value for  $\Gamma_s$  and  $\Gamma_L$  in order to satisfy the above requirements. Specify the value of  $G_T$  and the value of  $\Gamma_{out}$ .
- 2) (3p) Assuming a single stub matching network for the output network, draw the scheme of the network and evaluate its parameters.
- 3) (2p) Assuming at input a 2-tone signal, evaluate the maximum input power (Pin) determining at output the level of intermodulation lines 30 dB smaller than the main lines.

#### Solution

Exercise 1

Using the assigned frequencies:  $\lambda_1$ =16.57 cm,  $\lambda_2$ =16.04 cm. The powers received by the vehicle from the two BS are given by:

$$P_{R1} = P_{T_1} \frac{\lambda_1^2}{(4\pi D_1)^2} G_{BS} G_{VH} \cos^2(\theta_1), \quad P_{R2} = P_{T_2} \frac{\lambda_2^2}{(4\pi D_2)^2} G_{BS} G_{VH} \cos^2(\theta_2)$$

Then, imposing  $P_{R1}=P_{R2}$  and replacing  $\cos(\theta_1) = y_1/D_1$ ,  $\cos(\theta_2) = y_2/D_2$ :

$$\left(\frac{D_2}{D_1}\right)^4 = \left(\frac{y_2}{y_1}\right)^2 \frac{\lambda_2^2}{\lambda_1^2} \frac{P_{T_2}}{P_{T_1}} = K^2 \Longrightarrow K = 0.3673$$

The lengths  $D_1$  and  $D_2$  can be expressed as follows:

$$D_1 = \sqrt{(y_1)^2 + (x_A - x_1)^2}, \quad D_2 = \sqrt{(y_2)^2 + (x_2 - x_A)^2}$$

Replacing in the previous equation:

$$\frac{(y_2)^2 + (x_2 - x_A)^2}{(y_1)^2 + (x_A - x_1)^2} = K = 0.3673$$

Finally, the following 2<sup>nd</sup> degree equation in  $x_A$  is obtained:  $x_A^2(1-K) + 2x_A(K \cdot x_1 - x_2) + y_2^2 - K \cdot x_1^2 + x_2^2 - K \cdot y_1^2 = 0$ 

$$0.6327x_A^2 - 10.327x_A + 39.635 = 0$$

Solving, we get the two following solutions:  $x_{A1}=10.1506$  Km,  $x_{A2}=6.1715$  Km. The first solution must be discarded because >  $x_2$ , The received power at the handover finally results:  $P_{r1}=P_{r2}=1.7582e-09$  (-57.55 dBm)

The directivity gain D is expressed by:

$$D = \frac{4\pi}{\int_{0}^{\pi/2} \int_{-\pi/2}^{\pi/2} f(\mathcal{G}, \varphi) \sin(\theta) d\theta d\varphi} = \frac{4\pi}{\int_{0}^{\pi/2} \sin(\theta) d\theta} \int_{-\pi/2}^{\pi/2} \cos^2(\varphi) d\varphi = \frac{4\pi}{\left[1 \cdot \frac{\pi}{2}\right]} = 8$$

From the expression  $\eta D=10^{(5.5/10)}$ , we get  $\eta=0.4435$ 

#### Exercise 2



$$\begin{split} A_{fl} &= 1.023, \ A_{f2} &= 1.122 \quad T_{f1} = T_0 \left( 10^{A_{f1}/10} - 1 \right) = 6.75^{\circ}K, \ T_{f2} = T_0 \left( 10^{A_{f2}/10} - 1 \right) = 35.38^{\circ}K \\ T_{LNA} &= T_0 \left( 10^{NF/10} - 1 \right) = 171.3737^{\circ}K, \\ T_{eq} &= T_a + T_{f1} + A_{f1}T_{LNA} + \frac{A_{f1} \left[ T_{SSB}A_{f2} + T_{f2} \right]}{G_{LNA}} = 358.8979^{\circ}K \\ G_{LNA} &= \frac{A_{f1} \left[ T_{SSB}A_{f2} + T_{f2} \right]}{T_{eq} - \left( T_a + T_{f1} + A_{f1}T_{LNA} \right)} = 12.1173 \quad (10.834 \text{ dB}) \\ \text{To get R=100 Mbit/sec we must have:} \\ E_b / N_0 &= SNR - 10 \log \left( R/B \right) = 28 - 4.95 = 23.05 \text{ dB} \,. \\ \text{Removing the LNA and second filter:} \end{split}$$

$$\begin{split} T_{eq} &= T_a + T_{f1} + A_{f1} T_{SSB} = 358.8979^{\circ} K \\ T_{SSB} &= \frac{1}{A_{f1}} \Big\{ 358.8979 - \Big[ T_a + T_{f1} \Big] \Big\} = 197.4733^{\circ} K \end{split}$$

Exercise 3

- 1. Enter the S parameters on the S. C.  $\rightarrow$  Device potentially instable with MSG=12.2 dB
- 2. Draw the circle NF=1.5 dB and several circles with Gav<MSG until the one tangent to the noise circle is found: Gav=11.24 dB
- 3. Select  $\Gamma$ s on the tangent point:  $\Gamma$ s=0.55 $\angle$ -164.4
- Imposing the matching at the transistor output the transducer gain is made equal to the available gain. Select on the S.C.: S Param→ Optimum Gamma → Load: G<sub>T</sub>=11.24 dB, Γ<sub>L</sub>=0.505∠-175.8, NF=1.5 dB
- 5. Check that both  $\Gamma$ s and  $\Gamma_L$  are outside the instability regions (source and load)
- 6. Being the output of transistor matched, if a lossless output network is used,  $\Gamma_{out} = 0$ .
- 7. Using the S.C. the single-stub network parameters are found:  $\theta$ =27.45°, b=1.186.