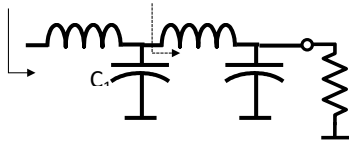


**RF SYSTEMS – 2<sup>nd</sup> part**  
**30 January 2018**

<b>Surname &amp; Name</b>
<b>Identification Number</b>
<b>Signature</b>

Exercise 1

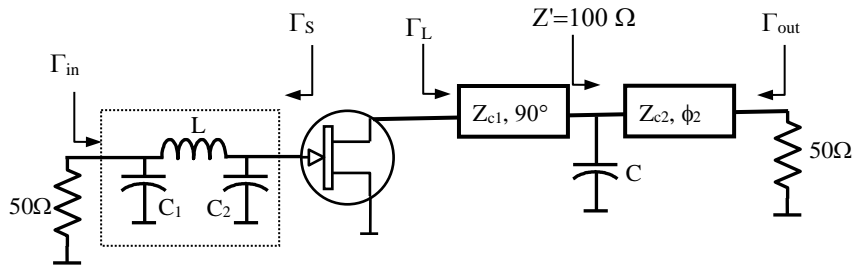
A matching network transforming  $150\Omega$  into  $75\Omega$  at 1GHz must be designed. The following scheme must be used (it is constituted by two cascaded L-shaped networks with lumped components, where the intermediate impedance is set to  $100\Omega$ ).



- 1) Evaluate  $L_1$ ,  $L_2$ ,  $C_1$  and  $C_2$
- 2) Propose an alternate solution giving the same impedances ( $100\Omega$  and  $75\Omega$ ), using only two distributed components

## Exercise 2

The following scheme shows a single stage power amplifier operating at 3 GHz.



The S parameters of the transistors are given as following:

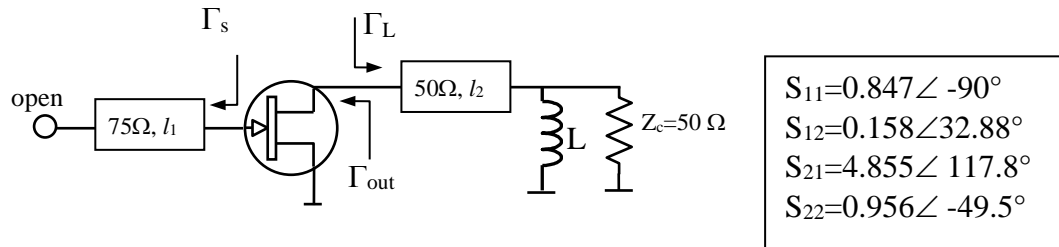
$$S_{11}=0.83\angle 149^\circ, S_{12}=0.076\angle 48^\circ, S_{21}=0.9\angle 9.3^\circ, S_{22}=0.62\angle 164.7^\circ$$

The transistor is pre-matched at input with a lumped network having the following components value:  $C_1=0.877$  pF,  $C_2=3.92$  pF,  $L=1.31$  nH.

- 1) Evaluate  $\Gamma_s$  and the corresponding value of  $\Gamma_L$  that determines the maximum transducer gain  $G_T$
- 2) Compute the value of  $G_T$
- 3) Design the output network imposing the intermediate impedance  $Z'$  real ( $100 \Omega$ ) and assigning  $Z_{c2}=100 \Omega$  (evaluate the parameters  $\phi_2$ ,  $C$  and  $Z_{c1}$ ). Note that the first line is an impedance inverter (approximate ( $\Gamma_L$  to a real number)
- 4) Evaluate the magnitude of the reflection coefficient at output ( $\Gamma_{out}$ ) of the amplifier
- 5) The above scattering parameters are measured at the operating power delivered to the load ( $P_L$ ). The transistor has  $P_{1dB}=33$  dBm and  $\Delta p=9$  dB. Knowing that the transistor is operating with 3 dB backoff, evaluate the mean power  $P_L$  delivered to load and the Carrier-to-Intermodulation CI (2-tone signal).

### Exercise 3

The following scheme refers to an oscillator working at unknown frequency. The S parameters of the transistor are also reported on the figure.



The input line ( $Z_c=75\Omega$ , length  $l_1$ , relative dielectric constant  $\epsilon_r=2.2$ ) is open circuited. It is known that  $l_1=12.64$  mm and  $\Gamma_s=-1$ .

- 1) Compute the oscillation frequency (hint: is the frequency determining  $\Gamma_s = -1$ ). Verify that the condition  $|\Gamma_{out}| > 1$  is satisfied.
- 2) Assign a suitable value for  $\Gamma_L$  and verify that all the conditions for starting the oscillation are fulfilled
- 3) Design the output network, i.e. compute the values of  $l_2$  and  $L$  (assume  $\epsilon_r=2.2$ )

# Solutions

Ex 1

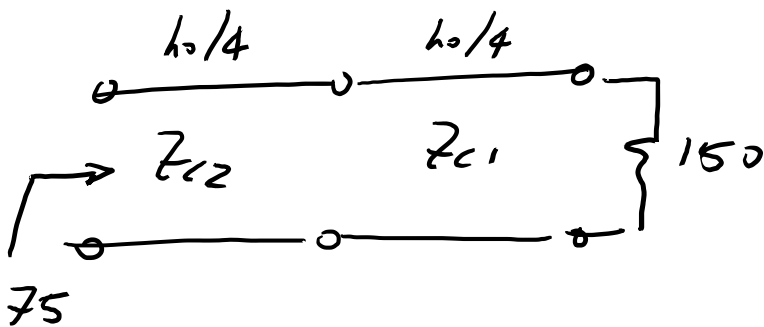
$$B_1 = \sqrt{\frac{1}{100} \left( \frac{1}{75} - \frac{1}{100} \right)} = \frac{1}{173.2} \Rightarrow C_1 = \frac{B_1}{2\pi f_0} = 0.92 \text{ pF}$$

$$X_1 = 75 \cdot 100 \sqrt{\frac{1}{100} \left( \frac{1}{75} - \frac{1}{100} \right)} = 43.3 \Rightarrow L_1 = \frac{X_1}{2\pi f_0} = 6.9 \text{ nH}$$

$$B_2 = \sqrt{\left( \frac{1}{100} - \frac{1}{150} \right) \frac{1}{150}} = \frac{1}{217.13} \Rightarrow C_2 = \frac{B_2}{2\pi f_0} = 0.75 \text{ pF}$$

$$X_2 = 150 \cdot 100 \sqrt{\frac{1}{150} \left( \frac{1}{100} - \frac{1}{150} \right)} = 70.7 \Rightarrow L_2 = \frac{X_2}{2\pi f_0} = 11.25 \text{ nH}$$

With distributed components:



$$Z_{c1} = \sqrt{150 \cdot 100} = 122.5 \Omega$$

$$Z_{c2} = \sqrt{100 \cdot 75} = 86.6 \Omega$$

## Ex 2

- 1) Using the S.C. we get  $\Gamma_S = 0.82 \angle -154.4^\circ$
- 2)  $(G_T)_{\max}$  is obtained by imposing the conjugate match at the trans. output. The optimum  $\Gamma_L$  is obtained with the S.C. :  $\Gamma_L = 0.653 \angle -179.9^\circ$   
 $G_T = 6.25 \text{ dB}$
- 3)  $Z_{C1}$  is obtained by imposing the transformation of  $100 \Omega$  into the real impedance  $R_L = \frac{(1 + \Gamma_L)}{1 - \Gamma_L} 50 = 125 \Omega \Rightarrow Z_{C1} = \sqrt{100 \cdot R_L} = 32.1 \Omega$   
 The remaining part of the network is a classical single stub matching network (all components normalized to  $100 \Omega$ ,  $\Gamma' = 0$ ).  
 With the S.C. we get :  $\phi_2 = 35.7^\circ$ ,  $b = 0.7$   
 $\Rightarrow C = \frac{b \cdot 0.01}{2\pi f} = 0.37 \text{ pF}$
- 4) The output is matched, then  $\Gamma_{\text{out}} = 0$
- 5)  $P_m = P_{1 \text{ dB}} - B.O. = 30 \text{ dBm}$   
 $B.O. = \frac{CF}{2} - \Delta_p - 3 \Rightarrow GI = 30 \text{ dB}$

### Ex 3

1) To get  $\Gamma_s = -1$  the line length must be  $\frac{h_0}{4}$  then:  $\rho_s = \frac{h_0}{4} = \frac{c}{4\pi f_0 \sqrt{\epsilon_2}}$

we get  $f_0 = 4 \text{ GHz}$

2) We compute  $\Gamma_{out}$  with the S.C.

imposing  $\Gamma_s = -1$ :  $\Gamma_{out} = 1.34 \angle -27.7^\circ$

Then  $Z_{out} = -1.95 - j2.9$  from which:

$$Z_L = +0.65 + j2.9 \quad (\Gamma_L = 0.88 \angle 36^\circ)$$

For this value of  $\Gamma_L$  we get  $|\Gamma_{in}| = 2.1$

oscillation OK!

3) Using the S.C. we get:

$$\phi_2 = 57.2^\circ = \beta l_2 \Rightarrow l_2 = \frac{57.2 \cdot c}{360 \cdot f_0 \sqrt{\epsilon_2}} = 8.03 \text{ mm}$$

$$b_L = -3.6 \Rightarrow \frac{1}{\omega_0 L} = 3.6 \cdot 0.02 \Rightarrow$$

$$\Rightarrow L = 0.55 \text{ nH}$$