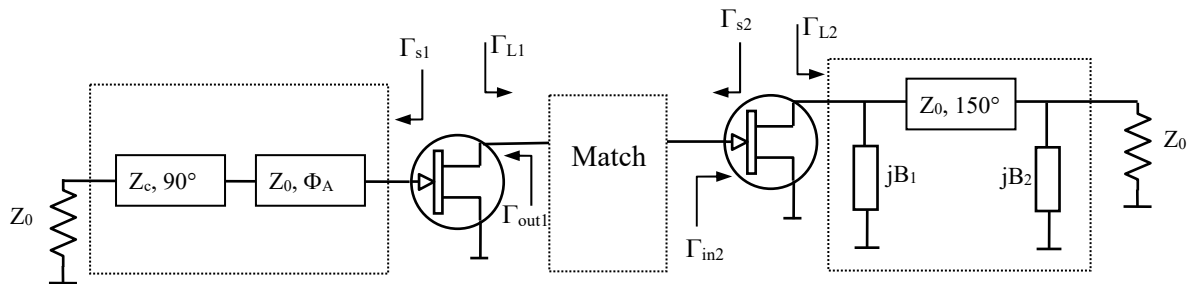


RF SYSTEMS – 2nd Midterm test
1th February 2017

Surname & Name
Identification Number
Signature

Exercise 1

The following scheme shows a 2 stage low noise amplifier operating at 12 GHz



The transistors are equal and are characterized by the following parameters ($Z_0=50 \Omega$):

$$S_{11}=0.569 \angle 78.2^\circ, \quad S_{12}=0.1 \angle -58.5^\circ, \quad S_{21}=3.226 \angle -52.1^\circ, \quad S_{22}=0.132 \angle 120.7^\circ$$

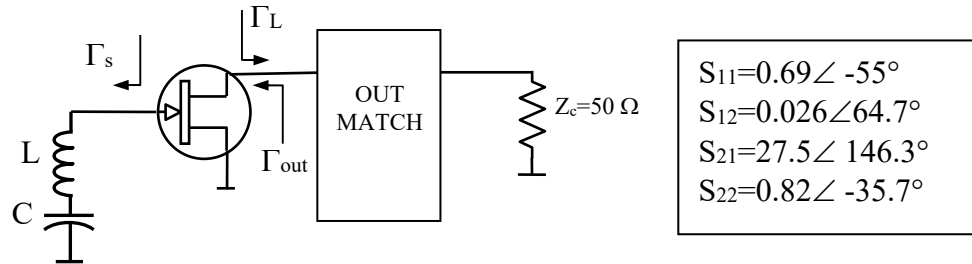
$$NF_{\min}=0.51 \text{ dB}, \quad \Gamma_{\min}=0.358 \angle -137.2^\circ, \quad r_n=0.12$$

The first stage must be designed for $NF=0.8 \text{ dB}$ while the second stage must be designed for the maximum transducer gain (compatibly with stability). It is also requested that the inter-stage network (“Match”) operates in conjugate matching both at input and output ($\Gamma_{L1}=\Gamma_{out1}^*$, $\Gamma_{s2}=\Gamma_{in2}^*$).

- 1) Evaluate Γ_{s1} , Γ_{L1} , Γ_{s2} , Γ_{L2} in order to fit the requirements
- 2) Compute the available gain of the two stages and the noise figure of the second stage
- 3) Compute the overall transducer gain and the overall noise figure of the amplifier (Hint: the overall available gain is the sum (in dB) of the available gain of the stages, then being the output matched...)
- 4) Design the input and output transforming networks. The parameters of the first are Z_c and Φ_A ; the unknowns of the second are B_1 and B_2 .

Exercise 2

The following scheme refers to an oscillator working at $f_{osc}=425$ MHz. The S parameters of the transistor are also reported on the figure.



The resonant circuit resonates at $f_{res}=400$ MHz, where it can be replaced with a short circuit.

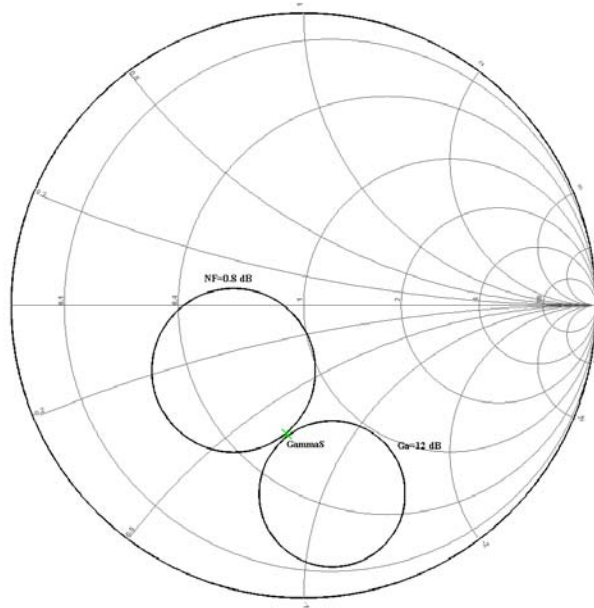
- 1) Imposing $|\Gamma_{out}|=1.3$ compute the values of Γ_s and Γ_L determining the start of oscillation
- 2) Verify that for $Z_s=0$ (short circuit) the start of oscillation is not possible. This happens at the resonance frequency f_{res} of the resonator.
- 3) Evaluate the values of L and C determining the requested value of Γ_s at $f_{osc}=425$ MHz and the resonance at $f_{res}=400$ MHz (Hint: the reactance of the series resonator is given by $X_s = \omega L - 1/\omega C$ with $\omega = 2\pi f$. The resonance frequency is given by $f_{res} = \frac{1}{2\pi\sqrt{LC}}$)
- 4) Chose a topology and design the output network

Solution

Exercise 1

Inserting the S parameters in the e-Smith Chart we discover that the transistors are unconditionally stable with $G_{Tmax}=12.788$, $\Gamma_{S,opt}=0.74\angle-81.4$, $\Gamma_{L,opt}=0.51\angle-155.2$.

1) The first stage must be however designed for $NF_1=0.8$, so we draw the circle with this NF value on the S. C. Then, in order to find the value of Γ_{s1} determining the maximum available gain compatible with the assigned NF, we draw some circles with $Ga=const (< G_{Tmax})$ and look for the one about tangent to the NF circle:



We found $Ga_1=11.96$ dB. The tangent point gives $\Gamma_{s1}=0.44\angle-97.9^\circ$. In order to get $Ga=GT$ we impose conjugate matching at the output of transistor 1 and we get (from the S.C.):

$\Gamma_{L1}=(\Gamma_{out1})^*=0.311\angle-135^\circ$. The second stage operates for the maximum transducer gain so it has $\Gamma_{s2}=\Gamma_{S,opt}$, $\Gamma_{L2}=\Gamma_{L,opt}$.

2) The overall Ga is the sum (in dB) of the Ga of the two stages (the second is equal to G_{Tmax}), so $Ga=Ga_1+G_{Tmax}=24.74$ dB. The noise figure of the second stage is obtained by assigning the current point on the S.C. equal to $\Gamma_{s2}=\Gamma_{S,opt}$ and asking for the optimum gamma load. We get $NF_2=2.53$ dB.

3) The overall transducer gain coincides with the overall Ga because the output of the second transistor is matched: $GT=Ga=24.74$ dB. The overall noise figure is given by the following formula:

$$(NF)_{TOT} = NF_1 + \frac{NF_2 - 1}{G_{a1}} = 10^{0.08} + \frac{10^{0.253} - 1}{10^{1.2}} = 1.252 \rightarrow 0.98 \text{ dB}$$

4) First network: we move on the circle with $|\Gamma|=|\Gamma_{s1}|$ toward the load up to the intersection with the real axis $\rightarrow \Phi_A=48.9^\circ$. The impedance seen in this point is $Z=2.571 \cdot 50=128.55 \Omega$. The characteristic impedance Z_c of the lambda/4 transformer is the given by $Z_c=\sqrt{128.55 \cdot 50}=80.17 \Omega$.

Second network: draw the circle $g=1$ rotated by 300° toward the source. Set the current point to Γ_{L2} and store in memory. Draw the circle $g=const$ passing for Γ_{L2} and select one intersection between the two circles ($\Gamma=0.385\angle172.69^\circ$). The value of imaginary part of ΔY with the sign reversed gives $b_1=1.537$. Give an increment to the current point Γ by 300° ; the new current point has $y=1+jb_2 \rightarrow b_2=-0.834$.

Exercise 2

Inserting the scattering parameter into the S.C. we discover the device potentially unstable and the suitable for an oscillator.

1) Draw the mapping circle for $|\Gamma_{out}|=1.3$ and select one of the intersection with the unit circle: $\Gamma_s=1\angle 132.31^\circ$. The corresponding reactance results $X_s=0.442\cdot 50=22.1\ \Omega$. Evaluate $\Gamma_{out}=1.3\angle -10.4 \rightarrow Z_{out}=-5.21-j3.53$. The assign $Z_L=1.7+j3.52$. Using the S.C. we enter this value as current point and compute $|\Gamma_{in}|=1.79$, so the oscillation start up is guaranteed.

2) Assigning $\Gamma_s=-1$ (short circuit) as current point we compute $|\Gamma_{out}|=0.957$ so the oscillation cannot start.

3) We have at $f_{osc}=425$ MHz: $X_s = \omega_{osc}L - \frac{1}{\omega_{osc}C} = \omega_{osc}L - \frac{\omega_{res}^2 L}{\omega_{osc}} = 22.1$. Replacing $\omega_{osc}=2\pi\cdot 425$

MHz and $\omega_{res}=2\pi\cdot 400$ MHz we get $L=72.48$ nH. Then $C = \frac{1}{\omega_{res}^2 L} = 2.18$ pF.

4) Using a single stub network: $\Phi=58.75^\circ$, $b=-2.73$.