

RF SYSTEMS
Mid-course Test - November 21th, 2016

Surname & Name
Identification Number
Signature

Exercise 1

It is given the following antenna directivity function: $f(\theta, \varphi) = \frac{\cos^2\left(\frac{\pi}{2} \cos\left(\theta + \frac{\pi}{2}\right)\right)}{\sin^2\left(\theta + \frac{\pi}{2}\right)}$.

The operating frequency is 3 GHz.

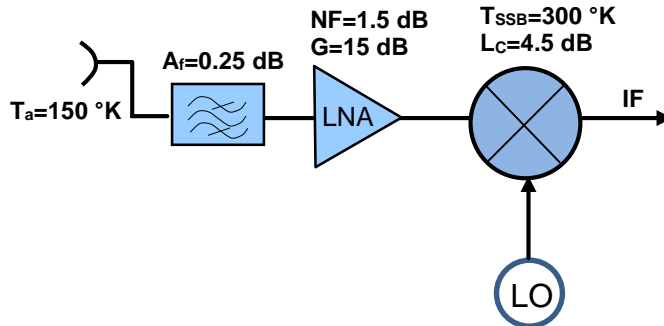
- 1) What is the direction θ_{MAX} for which $f=f_{max}=1$? Evaluate the 3dB beamwidth (θ_{3dB}) around this direction
- 2) Assuming that the emitted power is uniformly distributed on the spherical cap closing the cone of aperture $2\theta_B$ equal to θ_{3dB} , evaluate the directivity gain D_{MAX} .
- 3) It is known that $\frac{1}{r^2} \iint_{\Sigma} f(\theta, \varphi) \cdot d\Sigma = 1.745$ where Σ is the surface of the sphere of radius r centered on the antenna. Evaluate the exact value of D_{MAX} .
- 4) It is also known the radiation impedance $R_{rad}=50 \Omega$ and the efficiency factor $\eta=0.85$. Using the antenna in a receiver, evaluate the power P_L delivered to the receiver ($Z_L=50 \Omega$) when the incident power density S_R on the antenna is $2 \cdot 10^{-6} \text{ W/m}^2$.
- 5) Suppose that this antenna is used (both at T and R) in a communication system with transmitted power $P_T=30 \text{ dBm}$, equivalent noise temperature of the receiver $T_{eq}=350^\circ$, signal bandwidth $B=30 \text{ MHz}$:



Evaluate the maximum distance L for which the SNR at the receiver R is equal to 30 dB.

Exercise 2

Consider the following block diagram referring to the RF front-end of a receiver operating in the band 6-6.5 GHz (10 channels with 50 MHz width):



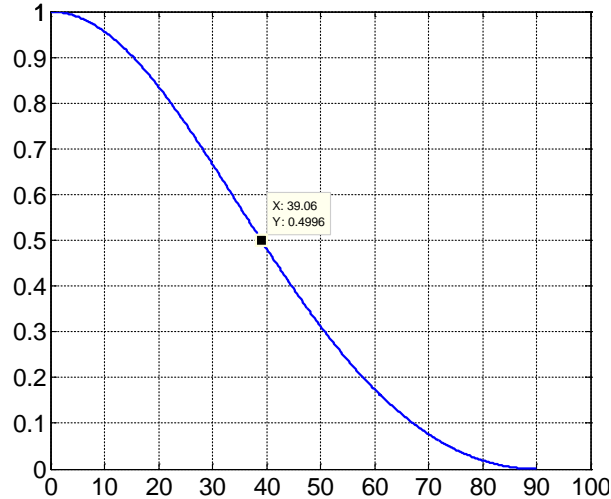
Assume the filter ideal in the stopband and equivalent to an attenuator (A_f) in the passband.

- 1) Assuming that the local oscillator operates at frequencies below the RF band (6-6.5 GHz), determine the range of the LO frequencies f_{OL} imposing the intermediate frequency $f_{IF}=470$ MHz.
- 2) What is the range of frequencies of the image band?
- 3) Evaluate the equivalent noise temperature T_{eq} of the RF front-end. Compute also the overall noise power at the mixer output (Assume the signal bandwidth $B=50$ MHz)
- 4) We know the minimum power density of the radiation incident on the antenna $S_R= 10^{-8}$ W/m². Evaluate the antenna gain G_A in order the signal-to-noise-ratio of the RF front-end is at least 15 dB (refer to the channel at $f_{RF}=6$ GHz)
- 5) Assume the receiver is tuned at $f_{RF}=6.425$ GHz and the received power at antenna output is $P_r=-80$ dBm. In the adjacent channel at $f_{ADJ}=6.375$ GHz there is a strong interference constituted by 2-tone spaced by 40 MHz (and centered at f_{ADJ}) and mean power $P_{ADJ}=-30$ dBm. Note that the LNA amplify both signals because they are in the tuning band (the interference at f_{ADJ} is finally removed by the IF filter)
 - a. Verify that one of the intermodulation tones produced in the LNA by the signal at f_{ADJ} falls inside the received channel (6.4-6.45 GHz)
 - b. Evaluate the minimum IP3 of LNA to get the $SNR=P_o/P_{int}=30$ dB, with P_o the power at f_{RF} at the LNA output and P_{int} the power in the intermodulation line.
 - c. Assuming the IIP3 of the mixer equal to 0 dBm evaluate the IIP3 of the whole RF front-end

Solution

Exercise 1

- 1) $\theta_{MAX} = 0^\circ$. Drawing graphically the function $f(\theta)$ it has:



From the graph $f(\theta)=0.5$ for $\theta=39.06^\circ$. Then $\theta_{3dB}=2*39.06=78.12^\circ$

$$2) D_{MAX} = \frac{2}{(1 - \cos(\theta_B))} = \frac{2}{\left(1 - \cos\left(\frac{\theta_{3dB}}{2}\right)\right)} = 8.955$$

$$3) (D_{MAX})_{exact} = \frac{4\pi}{\frac{1}{r^2} \iint_{\Sigma} f(\theta, \varphi) \cdot d\Sigma} = \frac{4\pi}{1.745} = 7.2$$

$$4) A_e = \frac{G \cdot \lambda^2}{4\pi} = \frac{\eta \cdot D_{max} \cdot \lambda^2}{4\pi} = \frac{0.85 \cdot 7.2 \cdot (3 \cdot 10^8 / 3 \cdot 10^9)^2}{4\pi} = 0.0049 \text{ m}^2$$

$$P_r = A_e S_R = 9.8 \cdot 10^{-9} \text{ W } (-50.09 \text{ dBm})$$

Being the receiver input matched to the antenna (loss resistance can be discarded),
 $P_L = P_r = -50.09 \text{ dBm}$

- 5) The Friis equation for the considered link is given by:

$$P_r = P_t - L_f + 10 \log(2\eta D_{MAX}) = 45.73 - L_f$$

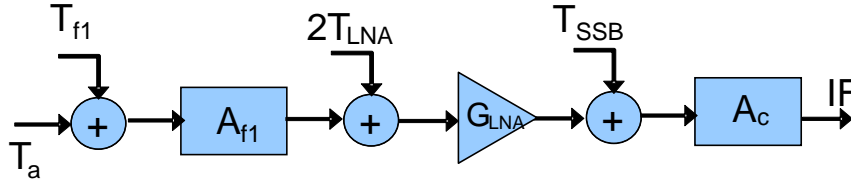
$$\text{with } L_f = 20 \cdot \log\left(\frac{4\pi L}{\lambda}\right) \text{ and } \lambda = 0.1 \text{ m.}$$

The noise power at the receiver input is $P_N = K \cdot T_{eq} \cdot B = 1.45 \cdot 10^{-13} \text{ W } (-98.39 \text{ dBm})$. Imposing $SNR = P_r / P_N = 30 \text{ dB}$ we get $P_r = -68.39 \text{ dBm}$. From the above equation:

$$L_f = 45.73 - (-68.39) = 114.12 \text{ dB} \rightarrow L = 4.04 \text{ Km.}$$

Exercise 2

- 1) The RF band is f_{IF} above f_{OL} , then $f_{OL}=f_{RF}-f_{IF}=5.53-6.03$ GHz
- 2) The image band is f_{IF} below f_{OL} , then $f_{IM}=f_{OL}-f_{IF}=5.06-5.56$ GHz
- 3) Consider the equivalent block diagram referring to noise temperature:



It has:

$$a_f=1.059, a_c=2.818 \quad T_f = T_0 \left(10^{A_f/10} - 1 \right) = 17.18^\circ K, \quad g_{LNA} = 31.62$$

Evaluation of T_{IF} :

$$T_{IF} = \left(T_a + T_f \right) \frac{g_{LNA}}{a_f a_c} + 2T_{LNA} \frac{g_{LNA}}{a_c} + T_{SSB} \frac{1}{a_c} = 4562.016 \text{ }^\circ K$$

The equivalent noise temperature at input:

$$T_{eq} = T_{IF} \frac{a_f a_c}{g_{LNA}} = 430.68 \text{ }^\circ K$$

- 4) The equivalent noise power at input is given by:

$$P_N = K \cdot T_{eq} \cdot B = 2.97 \cdot 10^{-13} \text{ W } (-95.27 \text{ dBm}).$$

Imposing $SNR = P_R - P_N = 15$ dB we get $P_R = -80.27$ dBm ($9.4 \cdot 10^{-12}$ W).

Being $P_R = A_e \cdot S_R \rightarrow A_e = 9.4 \cdot 10^{-4}$ m and $G = (4\pi/\lambda^2) A_e = 4.7236$ (6.74 dB)

The wavelength λ is given by $3 \cdot 10^8 / 6 \cdot 10^9 = 5 \cdot 10^{-2}$ m.

- 5) The intermodulation tones are located at $f_0 \pm 1.5\Delta = 6.375 \pm 0.06 = (6.435, 6.315)$. The first tone is inside the received channel.

The power received in the desired channel after the LNA is given by $P_0 = -80 - 0.25 + 15 =$

-65.25 dBm. The power P_{int} in the intermodulation line must be 30 dB below P_0 , then

$P_{int} = -95.25$ dBm. The power in adjacent channel at LNA output is $P'_{ADJ} = P_{ADJ} + G_{LNA} - A_f =$

-15.25 dBm (mean power). Imposing $P_{int} = 3(P'_{ADJ} - 3) - 2IP_3$, we obtain $IP_3 = (3(P'_{ADJ} - 3) - P_{int})/2 = 20.25$ dBm.

The overall IIP3 of the RF front-end can be derived from:

$$\left(\frac{1}{iip_3} \right)_{tot}^2 = \left(\frac{g_{LNA}}{a_f ip_{3,LNA}} \right)^2 + \left(\frac{g_{LNA}}{a_f iip_{3,MIX}} \right)^2 \rightarrow iip_{3,tot} = 0.0335 \text{ mW } (IIP_{3,tot} = -14.75 \text{ dBm})$$